

Memo: On normalization of visibility amplitudes in VLBI processing

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1 Amplitude normalization

The raw fringe amplitude has a number of biases. First bias is due to digitization. A general theory of digitization correction is developed by Kogan (1998). For a case of small amplitudes, i.e cross-correlation, the digitization correction does not act on the amplitude and is reduced to scaling: for a case of two-bit digitization the raw fringe amplitude has to be divided by 0.8825, for the case of 1-bit sampling has to be divided by 0.6366, and for a case of mixed 1-bit/2-bit sampling when one station records 2-bit and another records 1-bit the amplitude has to be divided by the scaling factor of 0.7495 in order to compensate distortion caused by digitization.

Digital correction of the autocorrelation is more complicated for two reasons. Firstly, for a case of large amplitudes the digital correction depends on amplitude and its functional dependence is not described by a simple scaling law. Secondly, the digital correction is defined for the correlation coefficient, not for the visibility spectrum, which is the Fourier transform of the lagged correlation. In order to perform digital correction of autocorrelation data, we do the following steps:

- put autocorrelation data in $[1, N]$ part of the array sized $[1, 2N]$, where N is the number of spectral channel in a given IF;
- compute autocorrelation at point $N+1$ by linear extrapolation: $A[N+1] = 2 \cdot A[N] - A[N-1]$;
- pad the remaining part of the extended autocorrelation array to zero: $A[N+2:2N] = 0.0$;
- perform Fourier transform of the extended autocorrelation array of dimension $2N$ and divide it by $2N$ for proper normalization: $a = \mathcal{F}(A)/(2N)$. Since the input autocorrelation is Hermitian, the output will have $N+1$ non-zero elements.
- compute the autoconvolution of the rectangular taper as $T(i) = 1 - (i - 1)/N$;
- normalize autocorrelation to 1 at zero lag: $T_n = a(1)$
- de-taper and normalize Fourier transform of the autocorrelation: $a_n[i] = a[i]/(T_n * T[i])$, which gives are the autocorrelation coefficient in lag domain;
- apply digital correction to the autocorrelation coefficient using tables computed by Kogan (1993a): $a_d[i] = D(a_n[i])$ for $i = 1, 2, \dots, N + 1$;
- Add symmetrical values of the lag correlation function in order to get real autocorrelation spectrum: $a_d[i] = a_d[2N + 2 - i]$ for $i = N + 2, N + 3, \dots, 2N$;

- Perform inverse Fourier transform of $a_d[i]$, which provides us the autocorrelation corrected for distortion due to digitization.

The explanation of the algorithm can be found in (Kogan, 1993b).

The correlator may also have biases in fringe amplitude. In order to calibrate for biases common for autocorrelation and cross-correlation, we compute average of autocorrelation amplitude over the IF bandwidth. For the perfect hardware and correlator this average value should be 1.0 according to Parseval theorem. It can deviate from 1.0 for several reasons. If the amplitude level of 2-bit sampling deviates from the optimal level, the 2-bit digitization correlation deviates from 0.8825. Old VLBA hardware correlator had a weird factor of 0.9028 for 1-1 bit sampling, 1.6834 for 2-2 bit sampling and 1.2347 for 1-2 bit sampling (Kogan, 1995). The origin of these factors is lost¹. The DiFX software correlator does not have these factors intrinsically, but it scales the visibility data by them to have raw amplitude as close as possible to the old hardware VLBA correlator. The SFXC software correlator does not apply these factors.

In order to correct visibility for scaling factors common for autocorrelation and cross correlation we divide cross-correlations by $\sqrt{\bar{A}_i \cdot \bar{A}_j}$, where \bar{A}_i is the mean autocorrelation corrected for digitization distortion averaged over both frequency and time. **NB:** even if we mask out a portion of the bandwidth, we average autocorrelation over the entire bandwidth regardless of mask.

There is a caveat related to the old VLBA hardware correlator. It was found that for high amplitudes (autocorrelation case), the internal correlator registers saturate. This saturation decreases the accumulated amplitude due to limited number of bits in the digital representation of the amplitude. Though, the saturation effect is negligible in cross correlation. The saturation is $1 + w/8$ for single polarization data and $1 + w/4$ for dual polarization data, where w the data weight defined as the ratio of the number of bits used to the total number of bits recorded. Since the saturation decreases the autocorrelation amplitude and since we have divided the cross-correlation amplitude by $\sqrt{\bar{A}_i \cdot \bar{A}_j}$, we need divide cross-correlation amplitude by the saturation factors in order to compensate cross-correlation amplitude.

The input FITS-IDI files have a field “CORRELAT” that supposed to designate the correlator. Unfortunately, this field is not always populated, so *PIMA* may not know which correlator generated the data. *PIMA* has keyword **FRIB.AMPL_FUDGE_TYPE** that specifies the correlator name directly (for instance DIFX or VLBA (for hardware correlator)). *PIMA* supports a variant of saturation calibration **VLBA_KOGAN** that $1 + 1/8$ for single polarization data and $1 + 1/4$ for dual polarization data, i.e. considering that weights do not affect the saturation calibration. It remains obscure which flavor of saturation calibration is better.

2 Bandpass computation

We consider that observed visibility $V_{12,\text{obs}}$ is related to the true visibility V_{12} with the ideal hardware as

$$V_{12,\text{obs}}(f) = V_{12,\text{ideal}}(f) B_1^*(f) \cdot B_2(f) \quad (1)$$

where B_i is a complex station-dependent function that describes distortion of the signal in the VLBI hardware² Typically, the amplitude response at a baseline is a tooth-like.

There are two factors that determine the amplitude response. First, the amplitude response of an individual IF to a signal with a flat spectrum distorts the input signal and makes its spectrum

¹I asked in 2013 Leonid Kogan who derived these factors what is their origin and he replied firmly: “I do not remember”.

²This definition describes the amplitude response to voltage. AIPS has the same convention. Alternatively one can define bandpass as the amplitude response to power.

non-flat. The autocorrelation spectrum describes the spectrum of a flat spectrum signal that passes through the VLBI hardware. Secondly, a signal at a given IF has an admixture of the signal from adjacent IFs, mainly at the edges of the IF band (see illustrations in the Appendix). This leaked signal is not coherent and causes decorrelation. Decorrelation is a function of frequency: it is greater at the edge of the IF. Therefore, a cross-correlation bandpass $B_1^*(f) \cdot B_2(f)$ in general is not equal to the product of autocorrelation bandpasses $\sqrt{A_1(f) \cdot A_2(f)}$.

The bandpass can be determined from observations of strong sources with continuum spectrum. We can neglect changes of the flux density over the intermediate frequency (IF) bandwidth and consider the spectrum flat, i.e frequency-independent. In that case the product of voltage bandpasses $B_1^*(f) \cdot B_2(f)$ is just the normalized cross-spectrum of the calibrator spectrum $\frac{1}{n} V_{12,\text{obs}}(f)$, where n is the normalization coefficient.

PLMA determines bandpass at a given polarization in three steps. At the first, so-called INIT step, *PLMA* examines results of the coarse fringe search and finds the observations with the greatest SNR at each baseline with the reference station. Initially, the so-called power baseline bandpass $B_{\text{ir,bas}} = \frac{1}{n_{\text{bas}}} V_{\text{ir,obs}}(f)$ is computed, where the normalization factor over the total IF band is

$$n_{\text{pow}}(B, f_l, f_h) = \frac{\int_{f_l}^{f_h} |B(f)| df}{f_h - f_l}, \quad (2)$$

where, f_l and f_h are the lower and upper frequencies of the IF, i.e. we require the normalized bandpass to have unity integral over the IF bandwidth. The visibility $V_{\text{ir,obs}}(f)$ used for bandpass computation are phase rotated with results of fringe fitting and averaged over time:

$$V_{\text{ir,obs}}(f) = \sum_k \sum_j v_k(f_j, t) e^{2\pi (f_0 \tau_p + f_0 \dot{\tau}_p (t_k - t_0) + (f_j - f_0) \tau_g + (f_j - f_0) \dot{\tau}_g (t_k - t_0))}, \quad (3)$$

where v_k is the raw visibility, τ_p is phase delay, τ_g is group delay, $\dot{\tau}_p$ and $\dot{\tau}_g$ are their time derivatives, f_0 and t_0 are the reference frequency and fringe reference time respectively. if the schedule had strong sources with SNR > 100, usually there is not need to average over frequency. If by oversight the schedule did not have strong sources, the IF is split into segments, and visibilities are coherently averaged over segments. The number of spectral channels within a segment is controlled by parameter **BPS.MSEG_ACCUM**. Value 1 means that no averaging is to be performed.

Since even for sources with the SNR > 1000 the visibility spectrum $V_{\text{ir,obs}}(f)$ has a noticeable scatter, *PLMA* smooths it with either using Legendre polynomial (**BPS.INTRP_METHOD: LEGENDRE**) or smoothing B-spline of the 3rd degree (**BPS.INTRP_METHOD: SPLINE**). Parameters **BPS.DEG_AMP** and **BPS.DEG_PHS** control the degree of the Legendre polynomial or the number of knots for the smoothing B-spline. When processing $V_{\text{ir,obs}}(f)$ phase, *PLMA* performs phase ambiguities resolution. Normalization is performed after smoothing.

Then the bandpass of the reference station is computed as

$$B_r(f) = \frac{1}{n_{\text{pow}}} (B, f_l, f_h) \left(\prod_i^{n-1} |B_{\text{ir,bas}}| \right)^{\frac{1}{2(n-1)}} \quad (4)$$

where normalization is computed the same was as in equation 2. The bandpass of the reference stations is set to the geometric mean of the bandpasses of all remote stations. Its phase is set to zero.

After we found the bandpass of the reference station, we compute voltage bandpasses from power bandpasses: $B_{\text{ir}} = \frac{1}{n_{\text{vol}}}(B_r, f_l, f_h)B_{\text{ir,bas}}/B_r f$. Voltage bandpass is normalized differently:

$$n_{\text{vol}}(B_i, B_r, f_l, f_h) = \frac{\int_{f_l}^{f_h} \sqrt{|B_i(f)| \cdot |B_r(f)|} df}{f_h - f_l}, \quad (5)$$

i.e. we require the square root of power of the product of the bandpasses at a given station and the reference station to have the integral over the IF bandwidth equal to unity.

The second step is computation of the bandpass in the so-called ACCUMULATIVE mode. First, *PLMA* finds the list of N observations with the highest SNR for each baseline with the references station. Parameter N is defined in parameter **BPS.NOBS_ACCUM** and does not count the observation used in the INIT mode. Fringe fitting for these observations is repeated and the phase bandpass computed in the INIT mode is applied to the observations before fringe fitting and the amplitude bandpass is applied after the fringe fitting. Expression “apply bandpass” means the visibilities of an observation are divided by the bandpass. Expression “apply phase bandpass” means the visibilities are divided by $B_1^* \cdot B_2 / (|B_1| |B_2|)$ and expression “apply amplitude bandpass” means the visibilities are divided by $|B_1| |B_2|$. Since we divide raw amplitudes by the product of amplitude bandpasses, this explains why we normalize the bandpasses at individual stations to the square root of power. It should be noted that the amplitude bandpass should never be applied before fringe fitting. Applying the amplitude bandpass before fringe fitting would have resulted to up-weighting visibilities at frequencies where the bandpass is small, i.e. at the edges of the bandwidth. Such up-weighting would have decreased the SNR.

After running fringe fitting in the accumulative mode, *PLMA* computes residual time-averaged complex visibilities normalized over (i.e. divided by) time and frequency. Had the bandpass been absolutely stable in time, the residual spectrum presented as a complex number would be (1.0, 0.0). *PLMA* computes the arithmetic average phase of normalized residuals R as $\Psi(f) = \sum R_i(f) / |R_i(f)| / n$ and geometric average of their amplitudes as $\kappa(f) = \prod |R_i(f)|^{1/n}$ and computes phase and amplitude of accumulative bandpass as $\Psi(f)$ and $1/n_{\text{vol}}(B_i, B_r, f_l, f_h) \kappa(f) / |B_r(f)|$ respectively. The amplitude of the stacked residual amplitude bandpass is divided by the amplitude of the INIT bandpass of the reference station and, thus, is transformed to the voltage bandpass. The bandpass of the reference station is not updated at this step.

The third step is computation of the bandpass in the so-called FINE mode using least squares. First, *PLMA* finds the list of K observations with the highest SNR for each baseline with the references station. Parameter K is defined by keyword **BPS.NOBS_FINE** and includes the observation used in the INIT mode. Similar to the previous step, the phase bandpass computed in the accumulative mode is applied before fringe fitting, the amplitude bandpass is applied after fringe fitting, and the normalized complex residuals $R(f)$ averaged over time are computed. Then the coefficients of the bandpass expansion for all stations are computed in a single least square solution. The phase bandpass is computed as

$$\sum b_{ir} P_j(f) = \frac{R_{ir}(f)}{|R_{ir}(f)|}. \quad (6)$$

where b_{ij} are the coefficients for the i -th station and $P_j(f)$ is the basic function. The amplitude bandpass is computed as

$$\sum a_i P_j(f) + a_r P_j(f) = \log |R_{ir}(f)|. \quad (7)$$

Here a_{ij} are the coefficients of expansion of the bandpass logarithm for stations with index i and r . After computation of the bandpass in FINE mode, *PLMA* computes residuals after applying this bandpass and identifies the observations with the largest root mean square phase residuals and the observations and the largest root mean square amplitude residuals. If the residuals exceed the limits specified by parameters **BPS.PHAS_REJECT** and **BPS.AMPL_REJECT**, *PLMA* removes such an observation from the bandpass computation and updates the least square solution. The iterations are performed till either the rms of residuals becomes less than **BPS.PHAS_REJECT** and **BPS.AMPL_REJECT**, or the number of remaining observation at a given baseline becomes **BPS.MINOBS_FINE**.

The final bandpasses for all stations but the reference one are renormalized once again using voltage renormalization.

The main reason why a three-step procedure is implemented in *PLMA* is to detect and mitigate the influence of bad observations on bandpass computation. It is not uncommon when observations with the largest SNR are affected by the radio interference (RFI). If only one observation is used for bandpass computation at a given baseline, i.e. bandpass computation is limited to the INIT mode, and that observation is affected by RFI, the bandpass will be suitable only for that observation, and all other observations will become affected by the influence of the RFI when corrupted bandpass is applied. Bandpass computation in the ACCUMULATIVE mode allows to dilute the influence of bad observations. Bandpass computation in the FINE mode allows to remove several bad observations from bandpass computation automatically mode and completely eliminate their influence. The three-step procedure also mitigates possible bandpass computation failures due to incorrectly resolved phase ambiguities. Phase ambiguities need be resolved only when processing the first observation in the INIT mode. All other steps use visibilities with applied phase bandpass, and the residual phases are supposed to be much smaller than 1/2 phase turn.

It is important to examine logs of bandpass computation. Statistics of residuals of bandpass computation allows us to make a judgment how stable the bandpass is over time. It may happen that due to a hardware reset bandpass at one or more stations is different for a portions of the experiment. At the moment, *PLMA* does not provide a convenient tool for processing observations with jumps in bandpasses. Processing such observations requires splitting the dataset into segments with stable bandpass and computing the bandpass for the segments separately.

I would like to emphasize that one of the most important part of VLBI data analysis is to compute a precise phase and amplitude bandpass. **It is a waste of time to process VLBI data with a poor bandpass!**

3 Bandpass renormalization

PLMA applies voltage normalization for bandpass. That normalization preserves the sum of amplitudes over frequency before and after applying the bandpass. This choice seems natural since it does not depend on specific knowledge of the hardware. However, this “natural” choice is often results in a bias. Two factors attenuate cross-correlation amplitude at the IF edges: the IF filter and the presence of signal from adjacent IFs that is not coherent. The central part of a bandpass is usually not affected. *PLMA* allows to specify the range of the bandwidth as representative and preforms renormalization. *PLMA* performs renormalization when it runs *splt* task. Keyword **SPLT.BPASS_NRML_METHOD** specifies whether to run renormalization and specifies **SPLT.BPASS_NRML_RANGE** the range of representative bandwidth as a fraction of the total bandwidth. **0.20:0.85** is a good choice for processing VLBA data with *rdbe_pfb* digital

filter setup. New normalization is computed as

$$n_{\text{ren}}(B_i, B_r, f_l, f_h) = \frac{\int_{f_l}^{f_h} M_i M_r \sqrt{|B_i(f)| \cdot |B_r(f)|} df}{\int_{f_l}^{f_h} M_i M_r df}, \quad (8)$$

where M_i and M_r are so-called fringe masks, i.e. masks used during fringe fitting. This choice of renormalization preserves the sum of amplitudes over frequency before and after applying the bandpass within the representative portion of the bandwidth, excluding the spectral channels that are masked out.

PLMA supports four masks: autocorrelation mask, bandpass mask, fringe mask and split mask. Fringe mask is applied during fringe fitting, except task *bpas*. Task *bpas* uses the bandpass mask for fringe fitting. Task *splt* uses split mask for computing time and frequency averaged visibilities. It is important to emphasize that just fringe mask is to be used for bandpass renormalization.

Applying bandpass renormalization usually results in an increase of image flux density. Such bandpass renormalization mitigates amplitude reduction due to decorrelation at the edges of the bandpass. Though, as Figures 1–2 show, the choice of the representative portion of the bandwidth is at some extent subjective. The subjectiveness in the selection of the representative portion of the bandpass may result in up-scaling or down-scaling flux densities at a level of several per cents.

4 Polarization bandpass

PLMA supports so-called polarization bandpass $P_i(f)$ that is defined this way:

$$\begin{aligned} V_{12,\text{obs}}^{RR}(f) &= V_{12,\text{ideal}}^{RR}(f) B_1^*(f) \cdot B_2(f) \\ V_{12,\text{obs}}^{LL}(f) &= V_{12,\text{ideal}}^{LL}(f) B_1^*(f) \cdot B_2(f) P_1^*(f) \cdot P_2(f) \cdot e^{2i(\psi_1(t) - \psi_2(t))}, \end{aligned} \quad (9)$$

where $\psi_i(t)$ is the feed horn rotation angle at the i -th station with respect to the local meridian. Using other language, the polarization bandpass is the averaged ratio of the spectrum of complex visibilities at LL polarization to the complex visibilities at RR polarization with phases corrected for the feed horn rotation.

When dual-band data are processed, *PLMA* treats RR data as the 1st polarization. It computes single-band RR bandpass using the procedure outlined above. When dual band are processed and keyword **POLARCAL_FILE** is not set to **NO**, *PLMA* for each step, INIT, ACCUM, FINE computes the corresponding polarization bandpass using the same observations as for RR bandpass. Thus, if **POLARCAL_FILE** is not set to **NO**, *PLMA* computes two bandpasses.

In the INIT mode *PLMA* first applies the RR INIT bandpass to RR data, computes residual spectrum $R^{RR}(f)$, then applies RR-bandpass to LL data, multiples visibilities by $e^{2i(\psi_1(t) - \psi_2(t))}$ to compensate the differences in the contribution of the feed-horn rotation angle to RR and LL visibilities and computes LL polarization residual spectrum R^{LL} . Then $P_{\text{ir,raw}} = R^{LL}/R^{RR}$. Then raw polarization bandpass is smoothed with Legendre polynomials or B-splines, transformed from power bandpass to voltage bandpass, and normalized the same way as RR-bandpass.

In the INIT mode *PLMA* applies the INIT polarization bandpass to LL-band residuals and get accumulative residuals: $P_{\text{ir,acc}}(f) = R^{LL}(f)/R^{RR}(f)/(P_i^*(f) \cdot P_r(f))$. These accumulative residuals are averaged out, as an arithmetic mean for phase part and as a geometric mean for the amplitude

part. The same voltage normalization is applied for the polarization bandpass as for the RR single polarization bandpass.

In the FINE mode *PLMA* applies the ACCUM polarization bandpass to LL-band residuals and get fine residuals. The parameters of the Legendre polynomial and or B-spline expansion coefficients for phase of the polarization bandpass for all stations, except the reference one and the parameters of the polynomial or B-spline expansion coefficients for logarithm of the amplitude polarization bandpass are evaluated with a single least square solution followed by identification the observations with the largest residual and their removal from the parameter estimation process.

Polarization bandpass allows to compute I-polarization visibilities on the fly before fringe fitting:

$$V_{12}^I(f) = \frac{1}{2} \frac{V_{12(f)}^{RR} + \frac{V_{12(f)}^{LL} e^{2i(\psi_1(t)-\psi_2(t))}}{\frac{P_1^*(f)}{|P_1(f)|} \cdot \frac{P_2(f)}{|P_2(f)|}}}{\frac{B_1^*(f)}{|B_1(f)|} \cdot \frac{B_2(f)}{|B_2(f)|}}. \quad (10)$$

I-polarization visibilities have approximately $\sqrt{2}$ higher SNR than RR or LL visibilities³, which makes them attractive for detection of weak sources. A general recommendation is always to use I-polarization combination of dual-polarization observables for fine fringe fitting. However, using I-polarization requires a correctly computed polarization bandpass.

Polarization bandpass re-normalization is performed differently:

$$n_{\text{ren}}(B_i, B_r, f_l, f_h) = \frac{\int_{f_l}^{f_h} M_i M_r \sqrt{|B_i(f)| \cdot |B_r(f)| \cdot |P_i(f)| \cdot |P_r(f)|} df}{\int_{f_l}^{f_h} M_i M_r df}, \quad (11)$$

Keyword **SPLT.POLAR** visibility for which polarizations should be written in the output file. When **SPLT.POLAR: I** *PLMA* task *splt* calibrates visibilities for all four polarizations:

$$\begin{aligned} V_{12}^{RR} &= \frac{V_{12}^{RR}}{B_1^* \cdot B_2} \\ V_{12}^{LL} &= \frac{V_{12}^{LL} e^{2i(\psi_1-\psi_2)}}{B_1^* \cdot B_2 \cdot P_1^* \cdot P_2} \\ V_{12}^{RL} &= \frac{V_{12}^{RL} e^{-2i\psi_2}}{B_1^* \cdot B_2 \cdot P_2} \\ V_{12}^{LR} &= \frac{V_{12}^{LR} e^{2i\psi_1}}{B_1^* \cdot B_2 \cdot P_1^*} \end{aligned} \quad (12)$$

PLMA does not put I combination of RR and LL polarizations in the output; it lets DIFMAP to generate such combinations. The feed horn rotation angle is applied to left-circular polarization data to compensate the difference in the sign of the feed horn rotation angle and is not applied to right-circular polarization data. So by convention, the polarization vector of left-circular polarization

³If amplitudes of RR and LL visibilities are very close to each other than the advantage is exactly $\sqrt{2}$.

data is aligned with the polarization vector of right circular polarization data and both have the contribution of the feed horn rotation angle with the sign that corresponds to the right-circular polarization visibilities.

5 Autocorrelation renormalization

In VLBI data analysis we do not calibrate amplitude directly, but calibrate the noise level measured from the total power of the received signal that is the sum of the receiver thermal noise, atmospheric emission, Earth’s surface emission that spills over to the receive, and the cosmological background radiation. The contribution from the observed source to the total power is usually negligible. If we apply mask, and usually we do, we cut some spectral channels. In general, the average power integrated over the used portion of the bandpass differs than the average power integrated over the entire IF bandwidth, since the IF bandpass is not rectangular. VLBI hardware always measures system temperature T_{sys} across the entire IF⁴. Therefore, T_{sys} computed for the total bandwidth is not equal to the effective T_{sys} that would have been measured had a portion of the bandwidth be masked out. Autocorrelation renormalization corrects T_{sys} for missing channels.

First, autocorrelation is corrected for digital distortion, then and smoothed with spectral channels that falls to autocorrelation mask down-weighted. The same algorithm for smoothing the autocorrelation is used as for smoothing the amplitude bandpass. It should be stressed that masking for autocorrelation renormalization has a different meaning than for fringe fitting or visibility splitting. In the latter case, masking means replacing the visibility data with zeroes with zero weights, i.e. effectively excluding them from fringe fitting or from contribution to the averaged visibility.

In the case of autocorrelation smoothing masking means only exclusion from the input to the smoothing algorithm. The autocorrelations in the masked channels after smoothing replaced with values interpolated from the remaining unmasked points. Then the autocorrelation normalization is computed as

$$n_a(i) = \frac{\sum_k M_k(i) A_k(i)}{\sum_k A_k(i)}, \quad (13)$$

where $A_k(i)$ is smoothed autocorrelation for the i -the station and $M_k(i)$ is the *fringe* mask. **NB:** autocorrelation and fringe masks are used for different purposes for autocorrelation renormalization. The fringe amplitude is divided by $\sqrt{n_a(i) n_a(i)}$.

The purpose of smoothing is to avoid distortion of autocorrelation renormalization due to internal RFI generated by the VLBI hardware. These narrow-band signals do not contribute to the power of the receiver noise that T_{sys} measures. *PIMA* silently adds frequencies at spectral channels of phase calibration to the autocorrelation mask. The peaks in the autocorrelation at the frequencies of phase calibration is the prominent feature. Since usually spectral resolution is not sufficient to resolve phase calibration signal, the peaks at phase calibration should be excluded from summation of power. The peaks due to phase calibration in the autocorrelation spectrum appear if the phase calibration unit is turned on and their appearance does not depend whether phase calibration is used in data analysis.

It should be noted that autocorrelation normalization is 1.0 if no fringe mask was applied.

⁴Some VLBI data terminals measure T_{sys} across the entire band. At the moment, in such cases *PIMA* assumes system temperature at a given IF is equal to the system temperature in the entire band as if it would have measured independently.

References

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A Appendix. Plots of normalized cross-correlation and autocorrelation amplitudes

Normalized cross-correlation amplitude is shown with **blue color**. Autocorrelation amplitude is shown in **red color**. Prominent features: attenuation of the signal at edges of the IF and presence of phase-calibration signal in autocorrelation plots.

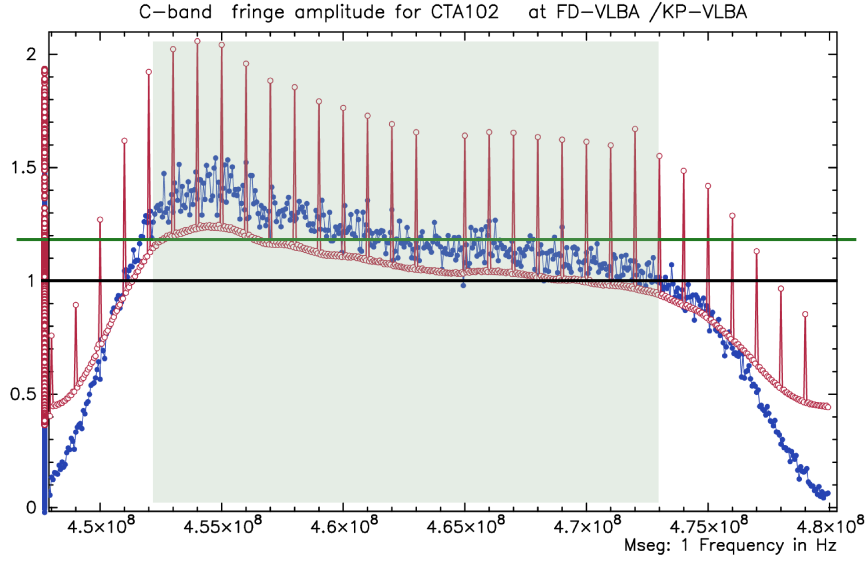


Figure 1: **cross-correlation** and **autocorrelation** of VLBA digital bandpass in the rdbe_pfb mode with 32 MHz wide IFs. The **thick black** line shows the bandpass average value over entire IF. The **green line** shows the average value over the representative portion of the IF bandwidth shown with the shadow area.

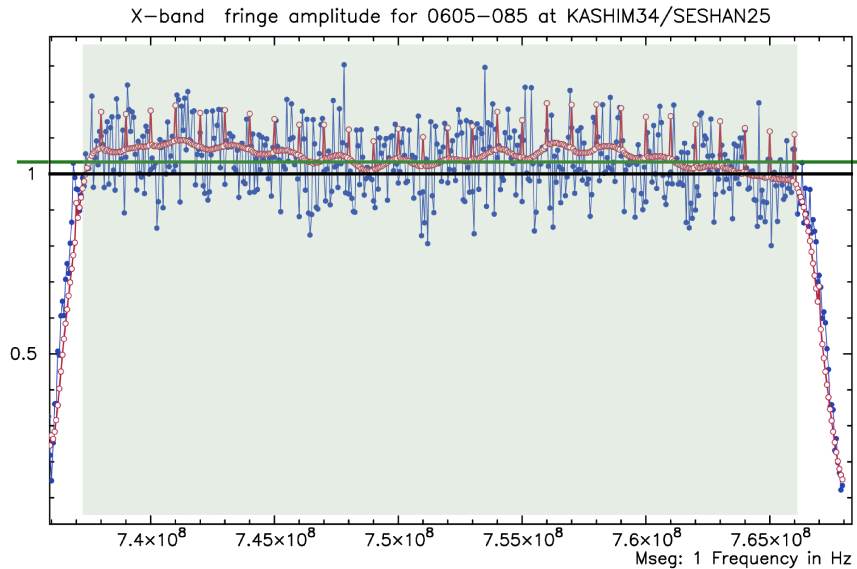


Figure 2: **cross-correlation** and **autocorrelation** of the CVN bandpass with 32 MHz wide IFs. The **thick black** line shows the bandpass average value over entire IF. The **green line** shows the average value over the representative portion of the IF bandwidth shown with the shadow area.

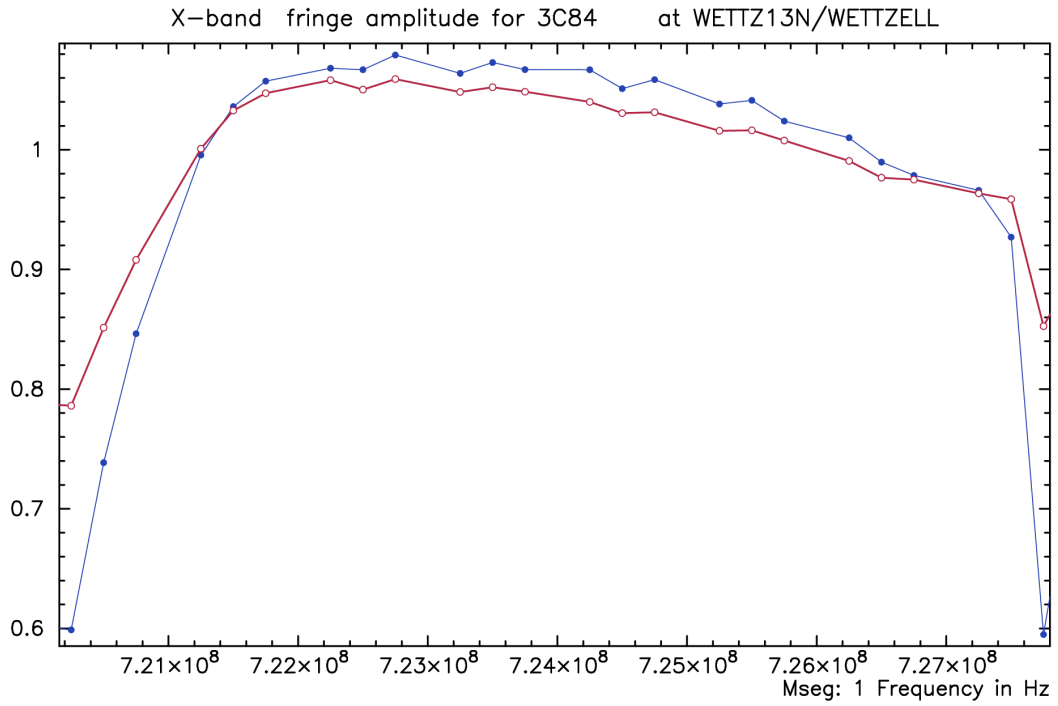


Figure 3: **cross-correlation** and **autocorrelation** of the IVS bandpass with 8 MHz wide IFs.

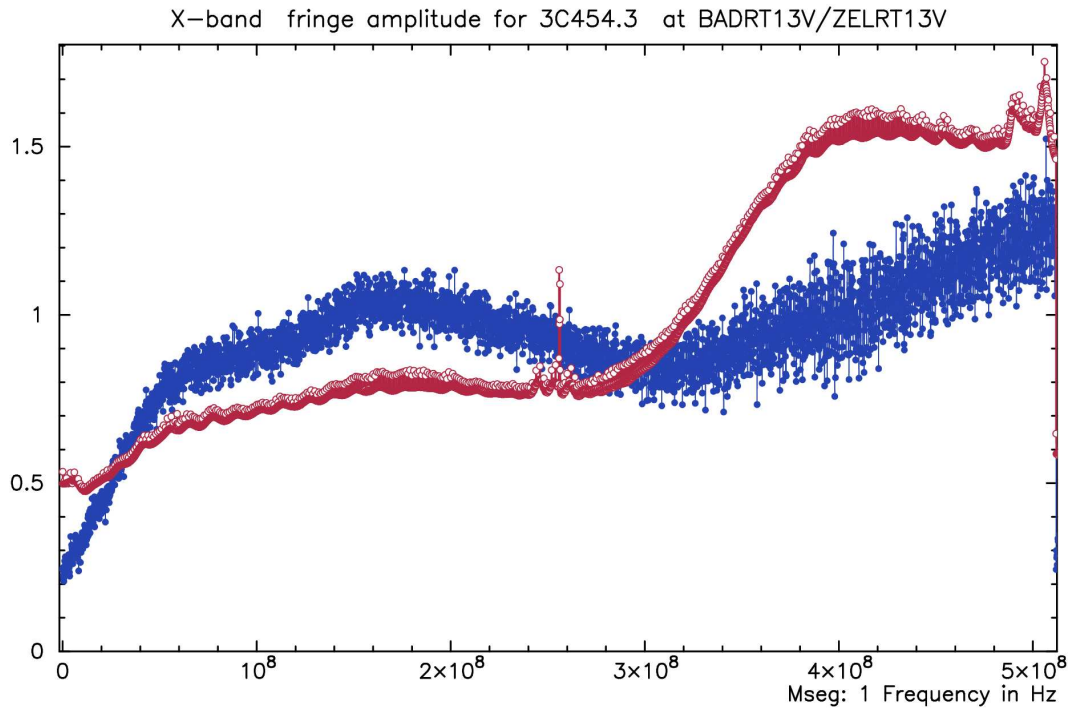


Figure 4: **cross-correlation** and **autocorrelation** of the IAA bandpass with 512 MHz wide IFs.